

# Supporting Information

## Structural Phase Transition and Bandgap Control through Mechanical Deformation in Layered Semiconductors 1T-ZrX<sub>2</sub> (X = S, Se)

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**Crystals synthesis:** Single crystals of 1T-ZrS<sub>2</sub> and 1T-ZrSe<sub>2</sub> were synthesized by chemical vapour transport method using I<sub>2</sub> as transport agent. Similar conditions as those presented in [37] have been used to grow large single crystals.

**High-pressure Raman and infrared spectroscopy:** Raman and infrared measurements were performed on the infrared beamline SMIS at the synchrotron SOLEIL. We used a DXR2 Thermo Fisher Raman microspectrometer equipped with a 633nm He-Ne laser as light source, a Peltier cooled CCD detector, a 600 grooves/mm grating, resulting in a spectral resolution of about 4 cm<sup>-1</sup>. Infrared measurements were performed on a custom-built horizontal microscope for diamond anvil cells (DACs), equipped with custom Cassegrain objectives, a MCT and a Si diode detectors, for the Mid-IR and the Near-IR respectively [1]. The horizontal microscope was coupled to Thermo Fisher iS50 interferometer with Quartz (NIR) / KBr (MIR) beamsplitters and synchrotron radiation as IR source.

Square samples of about 100 × 100 μm<sup>2</sup> were loaded into a membrane DAC with 400 μm culets. Stainless-steel gaskets were pre-indented to a thickness of about 50 μm and a hole of diameter 150 μm was drilled by electro-erosion. NaCl was used as pressure transmitting medium [2]. Pressure was measured in situ by the standard ruby fluorescence technique. Data was collected

every 1 GPa during both compression and decompression, with the last data point collected after the cell was open to release any residual pressure.

Sample thickness for optical transmittance experiments was determined before the measurement by means of optical interference, analyzing the oscillations of the transmitted light intensity as a function of wavelength (Fabry Perot interference). For the computation, the refractive index of the materials at energies below the bandgap is  $n = 4$  [3]. The value of the refractive index is experimentally determined through ellipsometry.

**X-ray diffraction:** The high-pressure X-ray diffraction experiments were performed at the X-ray diffraction platform of IMPMC at 0.85 GPa and 293 K, using a membrane diamond anvil cell (DAC) with a culet of 500  $\mu\text{m}$  in diameter. A 250  $\mu\text{m}$ -diameter hole was drilled in a stainless-steel gasket with a thickness of 200  $\mu\text{m}$  pre-indented to 80  $\mu\text{m}$ . The finely ground powders of  $\text{ZrSe}_2$  and  $\text{ZrS}_2$  were loaded into the gasket hole together with a ruby ball as pressure sensor [4] (R1 ruby fluorescence method). A 4:1 methanol-ethanol mixture was used as pressure transmitting fluid since it is known to provide hydrostatic conditions to approximately 10 GPa [5]. Before and after each measurement, pressure was determined by recording the ruby fluorescence spectra using a spectrometer with a 532 nm excitation laser. The calculated error for the pressure values is 0.1 GPa and the sensitivity was 0.05 GPa.

The DAC was then mounted on a Rigaku MM007HF diffractometer equipped with a Mo rotating anode ( $\lambda_{\text{K}\alpha 1} = 0.709319 \text{ \AA}$ ,  $\lambda_{\text{K}\alpha 2} = 0.713609 \text{ \AA}$ ), VariMax focusing optics and a RAXIS4++ image plate detector. X-ray data were collected at 20 °C. A  $\text{LaB}_6$  standard sample was measured in the same experimental conditions to calibrate the FIT2D program, the image processing software used to integrate the intensities around the Debye–Scherrer rings and to get the 1D patterns.

**Density Functional Theory Calculations:** Our first-principles calculations were performed at the density functional theory level as implemented in VASP [6,7]. We adopted the hybrid HSE06 [8] functional for describing the semiconducting systems, and the semilocal PBE functional for the metallic one [9]. Electron-core interactions were described through the projector augmented wave method, while Kohn-Sham wavefunctions were expanded in a plane wave basis set with a cutoff on kinetic energy of 400 eV. The integration over the Brillouin zone was carried out using a  $6 \times 6 \times 4$  ( $6 \times 4 \times 2$ ) k-mesh for the low-pressure (high-pressure) crystalline phase of  $\text{ZrSe}_2$ . We relied on the experimental crystal structures determined in our X-ray diffraction experiments.

## High-pressure Rietveld refinement of the XRD spectra

The crystal structure refinements were carried out using the Rietveld method as implemented in the Fullprof software [10].

Starting from the known cell parameters of  $\text{ZrS}_2$  and  $\text{ZrSe}_2$ , the refinements converged rapidly for the known structures at low pressure, considering low amounts of iron (diffraction from the DAC gasket).

For the two structures, preferred orientations were evidenced and their relative parameters refined: (001) for 1T- $\text{ZrS}_2$ , (-101) for HP- $\text{ZrS}_2$ , (001) for 1T- $\text{ZrSe}_2$ , and (010) for HP- $\text{ZrSe}_2$ .

The peak widths were significantly larger than the instrument resolution ( $\sim 0.15^\circ 2\theta$ ). Starting from an instrumental resolution function, Lorentzian isotropic size (Y) and Lorentzian isotropic strain (X) parameters were refined but only the second one (strain effect) improved the fits. Then, anisotropic refinements of strain parameters were attempted to get better peak profiles. The corresponding spherical harmonic coefficients are given in the following tables but the estimated standard deviations (esd) are too large to discuss the physical meaning of these values.

The low data to parameter ratio at high pressure - mainly due to the coexistence of starting and HP structure and to the peak broadening increasing with the strain - prevent us from a stable refinement of atomic positions.

Table 1. Results of the Rietveld refinement from X-ray diffraction analysis ( $\lambda_{\text{Mo}}$ ) of  $\text{ZrS}_2$ .

Pressure 0.37GPa			
<b>1T-ZrS<sub>2</sub></b>	<i>P</i> -3 <i>ml</i>	R <sub>Bragg</sub> = 9.93 %	Fract. (%) = 96 (4)
<i>a</i> = <i>b</i> = 3.6619 (11) Å <i>c</i> = 5.7746 (24) Å			
<i>V</i> = 67.059 (40) Å <sup>3</sup>			
<b>Strain Parameters (for profile only, large esd)</b>			
<i>S</i> <sub>400</sub> =3.21 (2.43), <i>S</i> <sub>004</sub> =11.11 (4.70), <i>S</i> <sub>112</sub> =0			
<b>Fe</b>	<i>I</i> <i>m</i> 3 <i>m</i>	R <sub>Bragg</sub> = 11.7 %	Fract. (%) = 4 (1)
<i>a</i> = 2.8771 (52) Å			
<i>V</i> = 23.816 (74) Å <sup>3</sup>			
Pressure 2GPa			
<b>1T-ZrS<sub>2</sub></b>	<i>P</i> -3 <i>ml</i>	R <sub>Bragg</sub> = 16.3 %	Fract. (%) = 93 (4)
<i>a</i> = <i>b</i> = 3.6365 (9) Å <i>c</i> = 5.6330 (19) Å			
<i>V</i> = 64.511 (31) Å <sup>3</sup>			
<b>Strain Parameters (for profile only, large esd)</b>			
<i>S</i> <sub>400</sub> =1.73 (1.96), <i>S</i> <sub>004</sub> =8.20(+/-3.71), <i>S</i> <sub>112</sub> =0			
<b>Fe</b>	<i>I</i> <i>m</i> 3 <i>m</i>	R <sub>Bragg</sub> = 30.2 %	Fract. (%) = 7 (1)
<i>a</i> = 2.8714 (39) Å			
<i>V</i> = 23.675 (56) Å <sup>3</sup>			
Pressure 4GPa			
<b>1T-ZrS<sub>2</sub></b>	<i>P</i> -3 <i>ml</i>	R <sub>Bragg</sub> = 12.1 %	Fract. (%) = 56 (5)
<i>a</i> = <i>b</i> = 3.6122 (7) Å <i>c</i> = 5.5275 (26) Å			
<i>V</i> = 62.461 (34) Å <sup>3</sup>			
<b>Strain Parameters (for profile only, large esd)</b>			
<i>S</i> <sub>400</sub> =1.25 (0), <i>S</i> <sub>004</sub> =5.67(4.86), <i>S</i> <sub>112</sub> =0.23 (11.30)			
<b>HP-ZrS<sub>2</sub></b>	<i>P</i> 2/ <i>m</i>	R <sub>Bragg</sub> = 17.8 %	Fract. (%) = 38 (8)
<i>a</i> = 6.4811 (104) Å	<i>b</i> = 3.7610 (10) Å	<i>c</i> = 5.0823 (126) Å	β= 108.922(50) deg
<i>V</i> = 117.188 (341) Å <sup>3</sup>			

**Strain Parameters (for profile only, large esd)**

$S_{400}=45$  (83),  $S_{040}=55$ (66),  $S_{004}=140$ (306),  $S_{220}=138$ (127),  $S_{202}=0$

$S_{022}=0$ ,  $S_{121}=0$ ,  $S_{301}=0$ ,  $S_{103}=0$

<b>Fe</b>	<i>I m3m</i>	$R_{\text{Bragg}} = 15.0 \%$	Fract. (%) = 6 (1)
$a = 2.8616$ (30) Å			
$V = 23.433$ (42) Å <sup>3</sup>			

**Pressure 6GPa**

<b>1T-ZrS<sub>2</sub></b>	<i>P -3m1</i>	$R_{\text{Bragg}} = 6.2 \%$	Fract. (%) = 37 (4)
$a = b = 3.5904$ (17) Å	$c = 5.4493$ (52) Å		
$V = 60.837$ (71) Å <sup>3</sup>			

**Strain Parameters (for profile only, large esd)**

$S_{400}=26$  (29),  $S_{004}=0$  (8),  $S_{112}=0$

<b>HP-ZrS<sub>2</sub></b>	<i>P 2<sub>1</sub>/m</i>	$R_{\text{Bragg}} = 11.6 \%$	Fract. (%) = 55 (6)
$a = 6.4766$ (63) Å	$b = 3.7235$ (25) Å	$c = 4.9906$ (75) Å	$\beta = 108.549$ (54) deg
$V = 114.100$ (218) Å <sup>3</sup>			

**Strain Parameters (for profile only, large esd)**

$S_{400}=45$  (28),  $S_{040}=146$ (52),  $S_{004}=46$ (60),  $S_{220}=88$ (90),  $S_{202}=124$  (104)

$S_{022}=0$ ,  $S_{121}=0$ ,  $S_{301}=0$ ,  $S_{103}=0$

<b>Fe</b>	<i>I m3m</i>	$R_{\text{Bragg}} = 7.1 \%$	Fract. (%) = 8 (1)
$a = 2.8587$ (34) Å			
$V = 23.363$ (48) Å <sup>3</sup>			

**Pressure 8GPa**

<b>1T-ZrS<sub>2</sub></b>	<i>P -3m1</i>	R <sub>Bragg</sub> = 8.7 %	Fract. (%) = 28 (6)
<i>a</i> = <i>b</i> = 3.5789 (28) Å	<i>c</i> = 5.4162 (99) Å		
<i>V</i> = 60.081 (128) Å <sup>3</sup>			

**Strain Parameters (for profile only, large esd)**

$S_{400}=109$  (85),  $S_{004}=63$  (69),  $S_{112}=126$  (138)

<b>HP-ZrS<sub>2</sub></b>	<i>P 2<sub>1</sub>/m</i>	$R_{\text{Bragg}} = 15.0 \%$	Fract. (%) = 62 (8)
$a = 6.4791$ (80) Å	$b = 3.7064$ (41) Å	$c = 5.0004$ (123) Å	$\beta = 108.88$ (11) deg
$V = 113.620$ (337) Å <sup>3</sup>			

**Strain Parameters (for profile only, large esd)**

$S_{400}=64$  (26),  $S_{040}=169$  (65),  $S_{004}=262$  (126),  $S_{220}=162$  (109),  $S_{202}=0$

$S_{022}=0$ ,  $S_{121}=0$ ,  $S_{301}=0$ ,  $S_{103}=0$

<b>Fe</b>	<i>I m3m</i>	$R_{\text{Bragg}} = 10.1 \%$	Fract. (%) = 10 (1)
$a = 2.8641$ (29) Å			
$V = 23.493$ (41) Å <sup>3</sup>			

**Pressure 10GPa**

<b>1T-ZrS<sub>2</sub></b>	<i>P -3m1</i>	$R_{\text{Bragg}} = 12.3 \%$	Fract. (%) = 28 (11)
$a = b = 3.5563$ (14) Å $c = 5.3731$ (90) Å			
$V = 58.850$ (104) Å <sup>3</sup>			

**Strain Parameters (for profile only, large esd)**

$S_{400}=155$  (172),  $S_{004}= 383$  (299),  $S_{112}= 0$

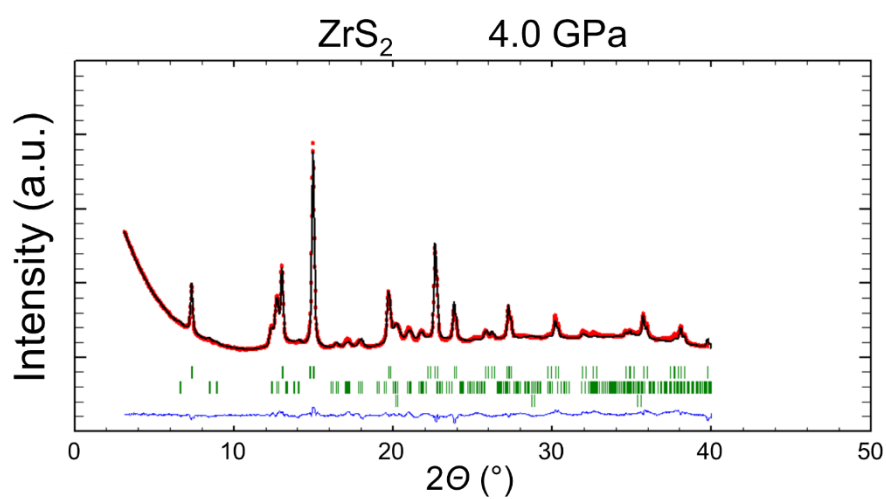
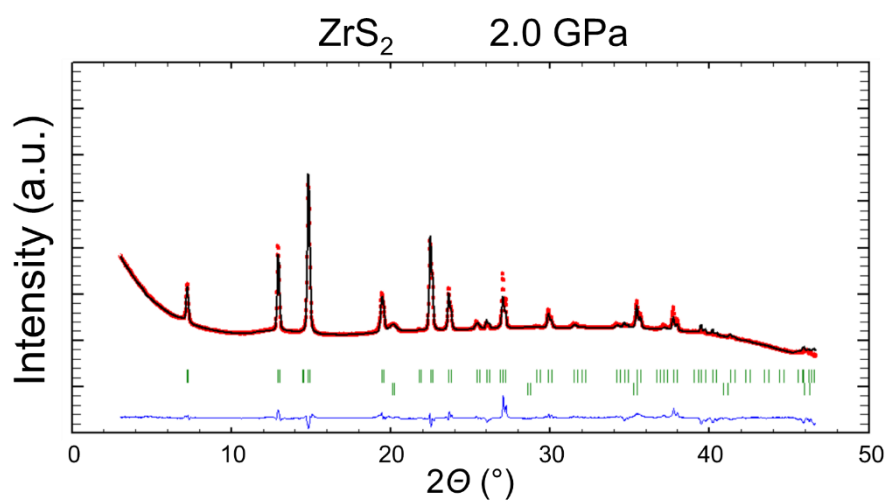
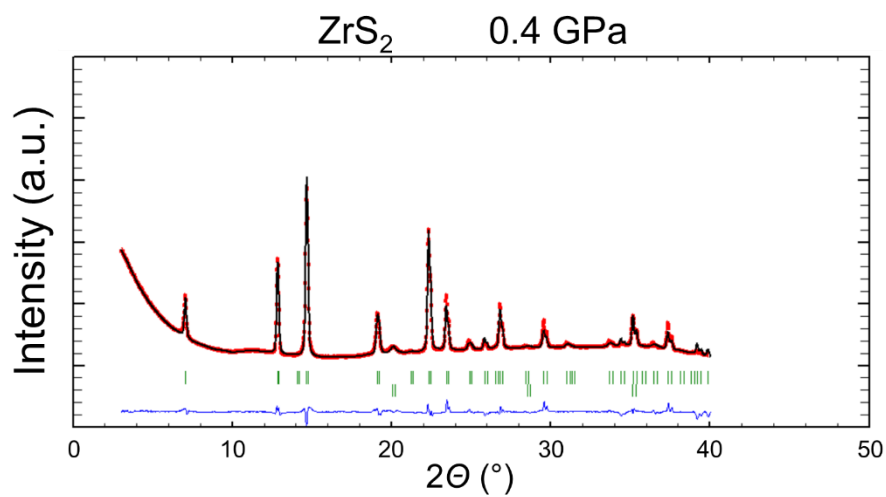
<b>HP-ZrS<sub>2</sub></b>	<i>P 2<sub>1</sub>/m</i>	$R_{\text{Bragg}} = 15.6 \%$	Fract. (%) = 65 (9)
$a = 6.4673$ (94) Å	$b = 3.6731$ (21) Å	$c = 4.9983$ (138) Å	$\beta = 109.23(13)$ deg
$V = 112.106$ (355) Å <sup>3</sup>			

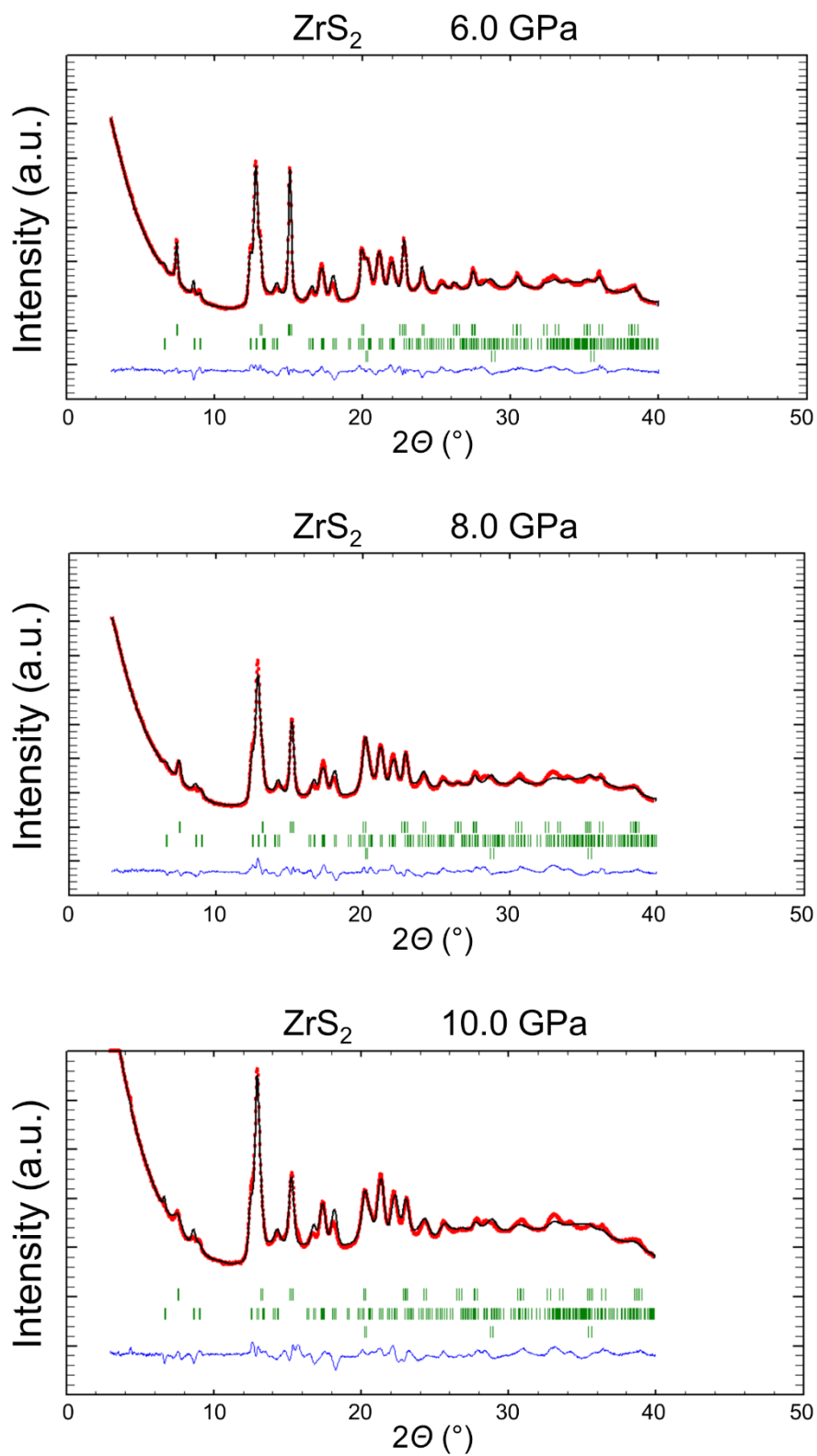
**Strain Parameters (for profile only, large esd)**

$S_{400}=11$  (22),  $S_{040}=200$  (64),  $S_{004}=125$  (118),  $S_{220}=210$  (85),  $S_{202}= 286$  (134)

$S_{022}=0$ ,  $S_{121}=0$ ,  $S_{301}=0$ ,  $S_{103}=0$

<b>Fe</b>	<i>I m3m</i>	$R_{\text{Bragg}} = 8.9 \%$	Fract. (%) = 7.1 (2)
$a = 2.8558$ (31) Å			
$V = 23.290$ (44) Å <sup>3</sup>			





**Figure SI 1** Results of the Rietveld refinement from X-ray diffraction analysis ( $\lambda_{\text{Mo}}$ ) of  $\text{ZrS}_2$ .



Table X. Results of the Rietveld refinement from X-ray diffraction analysis ( $\lambda_{\text{Mo}}$ ) of ZrSe<sub>2</sub>.

Pressure 0.4GPa			
<b>1T-ZrSe<sub>2</sub></b>	<i>P -3m1</i>	R <sub>Bragg</sub> = 7.72 %	Fract. (%) = 98 (8)
$a = b = 3.7656$ (2) Å	$c = 6.0953$ (30) Å		
$V = 74.854$ (37) Å <sup>3</sup>			
<b>Strain Parameters (for profile only, large esd)</b>			
$S_{400}=1.16$ (34), $S_{004}=5.76$ (4.31), $S_{112}=3.32$ (4.50)			
<b>Fe</b>	<i>I m3m</i>	R <sub>Bragg</sub> = 6.65 %	Fract. (%) = 2 (2)
$a = 2.8756$ (8) Å			
$V = 23.779$ (11) Å <sup>3</sup>			
Pressure 1.7GPa			
<b>1T-ZrSe<sub>2</sub></b>	<i>P -3m1</i>	R <sub>Bragg</sub> = 8.28 %	Fract. (%) = 98 (10)
$a = b = 3.7335$ (13) Å	$c = 6.0164$ (71) Å		
$V = 72.629$ (92) Å <sup>3</sup>			
<b>Strain Parameters (for profile only, large esd)</b>			
$S_{400}= 0.51$ (18), $S_{004}= 5.68$ (4.33), $S_{112}= 3.19$ (4.30)			
<b>Fe</b>	<i>I m3m</i>	R <sub>Bragg</sub> = 7.07%	Fract. (%) = 2 (2)
$a = 2.8486$ (10) Å			
$V = 23.114$ (14) Å <sup>3</sup>			
Pressure 3.3GPa			
<b>1T-ZrSe<sub>2</sub></b>	<i>P -3m1</i>	R <sub>Bragg</sub> = 10.5 %	Fract. (%) = 99 (7)
$a = b = 3.7213$ (2) Å	$c = 5.8494$ (24) Å		
$V = 70.150$ (29) Å <sup>3</sup>			
<b>Strain Parameters (for profile only, large esd)</b>			
$S_{400}= 1.20$ (27), $S_{004}= 4.11$ (3.13), $S_{112}= 0.22$ (3.07)			
<b>Fe</b>	<i>I m3m</i>	R <sub>Bragg</sub> = 4.07 %	Fract. (%) = 1 (3)
$a = 2.8215$ (56) Å			
$V = 22.462$ (8) Å <sup>3</sup>			
Pressure 5.2GPa			

**1T-ZrSe<sub>2</sub>** *P -3m1*  $R_{\text{Bragg}} = 14.4 \%$  Fract. (%) = 99 (6)  
 $a = b = 3.6909 (2) \text{ \AA}$   $c = 5.7716 (27) \text{ \AA}$   
 $V = 68.090 (33) \text{ \AA}^3$

**Strain Parameters (for profile only, large esd)**

$S_{400} = 15.32 (2.45)$ ,  $S_{004} = 55.78 (14.19)$ ,  $S_{112} = 0$

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**Fe** *I m3m*  $R_{\text{Bragg}} = 3.90 \%$  Fract. (%) = 1(1)  
 $a = 2.7942 (9) \text{ \AA}$   
 $V = 21.817 (12) \text{ \AA}^3$

**Pressure 7.4GPa**

**1T-ZrSe<sub>2</sub>** *P -3m1*  $R_{\text{Bragg}} = 10.2 \%$  Fract. (%) = 58 (5)  
 $a = b = 3.6473 (9) \text{ \AA}$   $c = 5.7208 (1) \text{ \AA}$   
 $V = 65.907 (24) \text{ \AA}^3$

**Strain Parameters (for profile only, large esd)**

NR

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**HP-ZrSe<sub>2</sub>** *I mmm*  $R_{\text{Bragg}} = 14.3 \%$  Fract. (%) = 41 (2)  
 $a = 3.6097 (20) \text{ \AA}$   $b = 5.3843 (82) \text{ \AA}$   $c = 12.1040 (103) \text{ \AA}$   
 $V = 235.252 (432) \text{ \AA}^3$

**Strain Parameters (for profile only, large esd)**

$S_{400} = 6.98(7.71)$ ,  $S_{040} = 21.10 (31.36)$ ,  $S_{004} = 1.43 (1.44)$ ,  $S_{220} = 10.68 (72.44)$ ,  $S_{202} = 0$ ,  $S_{022} = 0$

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**Fe** *I m3m*  $R_{\text{Bragg}} = 3.16 \%$  Fract. (%) = 1(1)  
 $a = 2.7664 (0.0032) \text{ \AA}$   
 $V = 21.171 (42) \text{ \AA}^3$

**Pressure 9.5GPa**

**1T-ZrSe<sub>2</sub>** *P -3m1*  $R_{\text{Bragg}} = 13.3 \%$  Fract. (%) = 39 (5)  
 $a = b = 3.6189 (16) \text{ \AA}$   $c = 5.7208 (2) \text{ \AA}$   
 $V = 64.886 (41) \text{ \AA}^3$

**Strain Parameters**

NR

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**HP-ZrSe<sub>2</sub>** *I mmm*  $R_{\text{Bragg}} = 13.9 \%$  Fract. (%) = 61 (8)  
 $a = 3.5824 (21) \text{ \AA}$   $b = 5.3699 (84) \text{ \AA}$   $c = 12.0613 (233) \text{ \AA}$   
 $V = 232.023 (592) \text{ \AA}^3$

**Strain Parameters (for profile only, large esd)**

$S_{400} = 0.48 (41)$ ,  $S_{040} = 1.03 (1.55)$ ,  $S_{004} = 0.09 (7)$ ,  $S_{220} = 1.55 (3.81)$ ,  $S_{202} = 0$ ,  $S_{022} = 0$

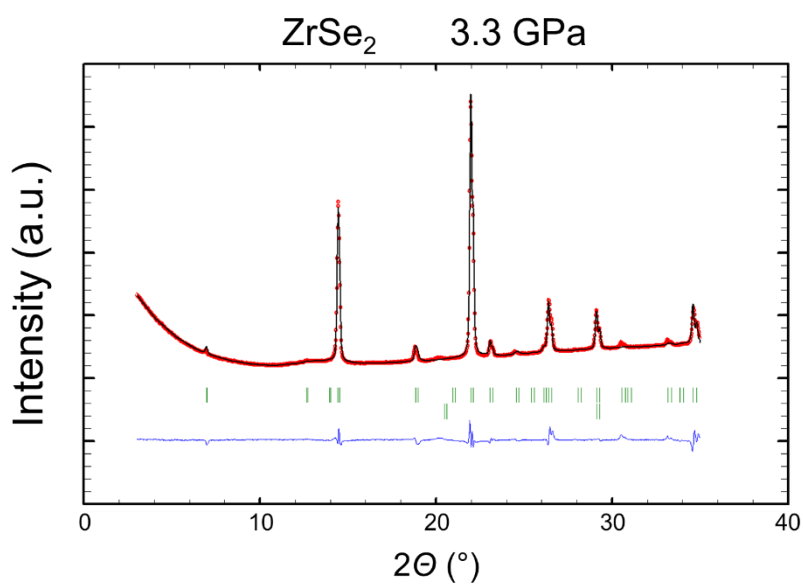
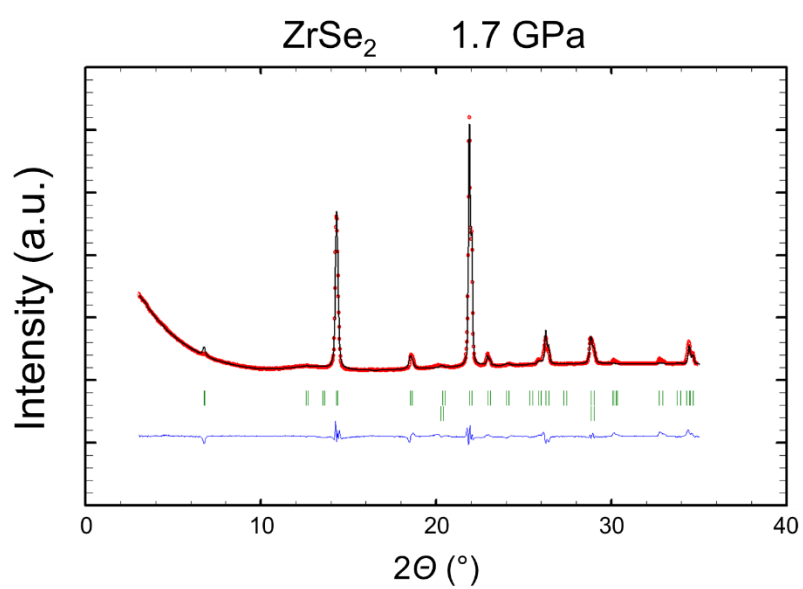
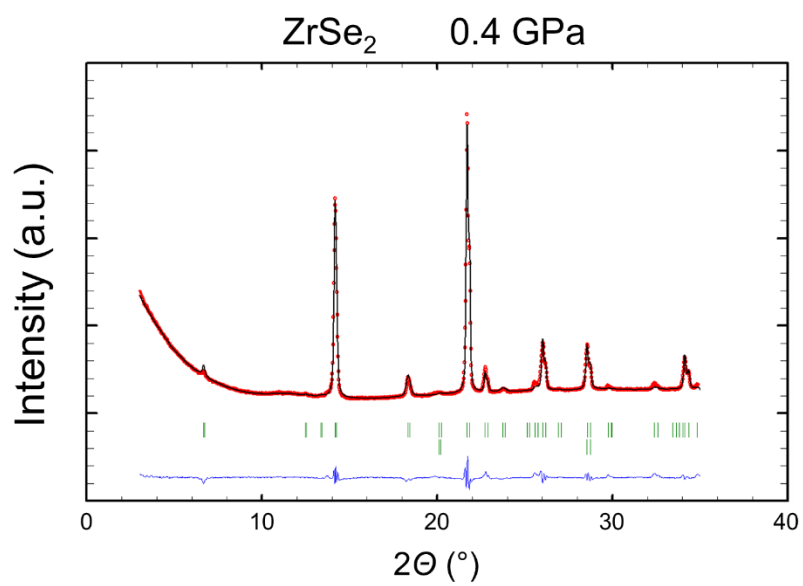
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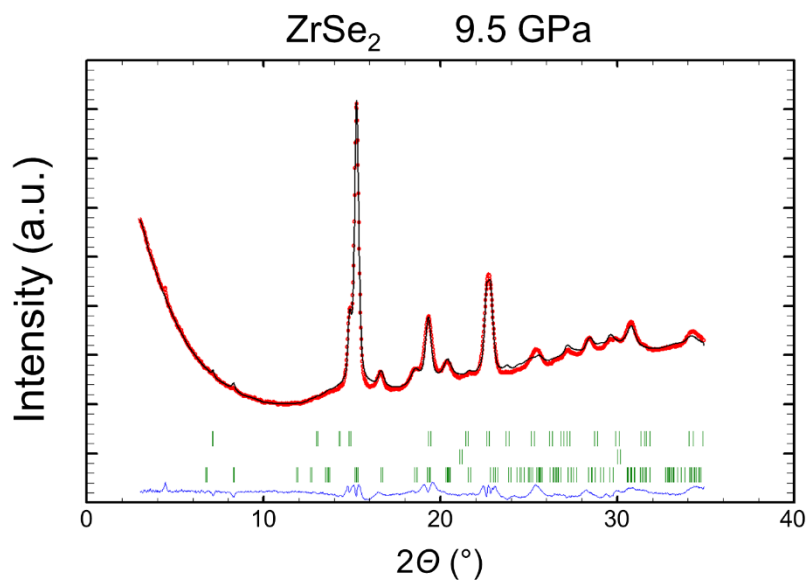
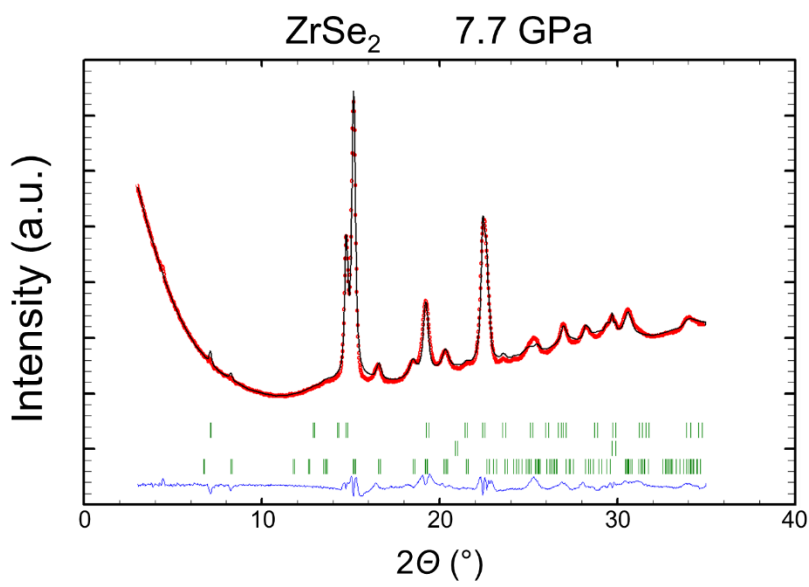
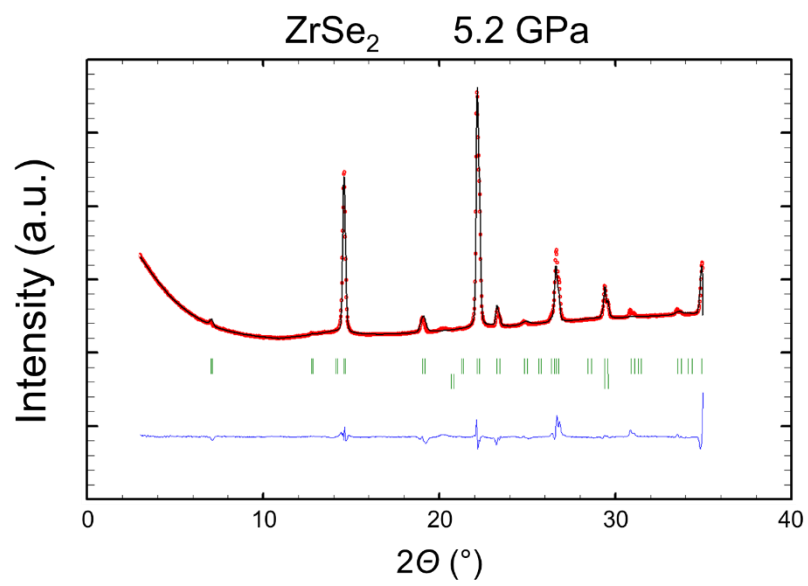
**Fe** *I m3m*  $R_{\text{Bragg}} = 0.5 \%$  Fract. (%) = 0 (1)  
 $a = 2.7413 (497) \text{ \AA}$

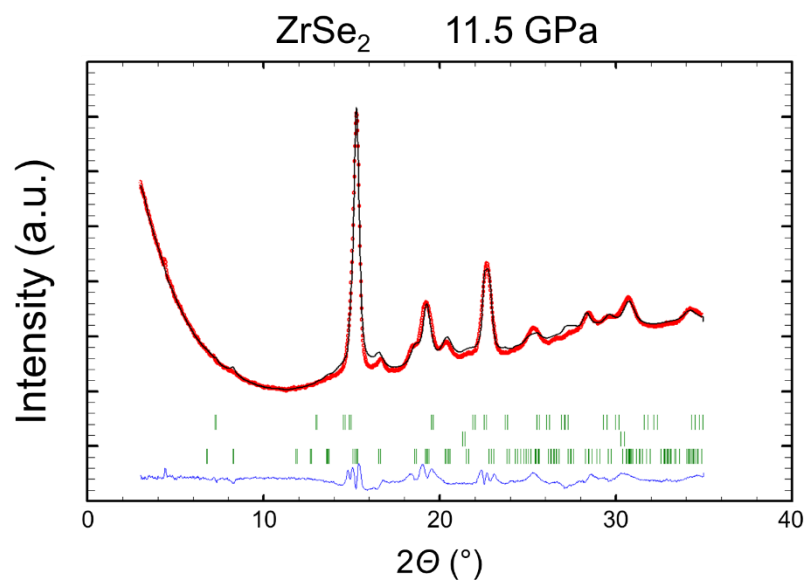
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$$V = 20.599 (647) \text{ \AA}^3$$

Pressure 11.5GPa			
<b>1T-ZrS<sub>2</sub></b>	<i>P -3ml</i>	R <sub>Bragg</sub> = 17.1 %	Fract. (%) = 19(3)
$a = b = 3.6307 (22) \text{ \AA}$	$c = 5.6089 (501) \text{ \AA}$		
$V = 64.031 (574) \text{ \AA}^3$			
<b>Strain Parameters</b>			
NR			
<hr/>			
<b>HP-ZrS<sub>2</sub></b>	<i>I mmm</i>	R <sub>Bragg</sub> = 15.4 %	Fract. (%) = 81 (10)
$a = 3.5894 (239) \text{ \AA}$	$b = 5.4119 (111) \text{ \AA}$	$c = 12.0219 (116) \text{ \AA}$	
$V = 233.527 (552) \text{ \AA}^3$			
<b>Strain Parameters (for profile only, large esd)</b>			
$S_{400} = 1.09(0.74), S_{040} = 2.03 (2.72), S_{004} = 0.07 (0.08), S_{220} = \text{NR}, S_{202} = 0.67 (0.68), S_{022} = 0$			
<hr/>			
<b>Fe</b>			
<b>not refined</b>	<i>I m3m</i>	R <sub>Bragg</sub> = NR	Fract. (%) = NR
<b>(too much overlap)</b>			
$a = \text{NR}$			
$V = \text{NR}$			







**Figure SI 2** Results of the Rietveld refinement from X-ray diffraction analysis ( $\lambda_{\text{Mo}}$ ) of  $\text{ZrS}_2$ .

### Pressure - Strain relation

Given the experimental X-ray diffraction (XRD) data, recorded during high-pressure experiments, it is possible to compute the change in unit cell parameters of the 1T-phases of  $\text{ZrS}_2$  and  $\text{ZrSe}_2$ . The data were used to compute the pressure – strain relation for the material.

The engineering strain (in percentage) applied to the material is computed as:

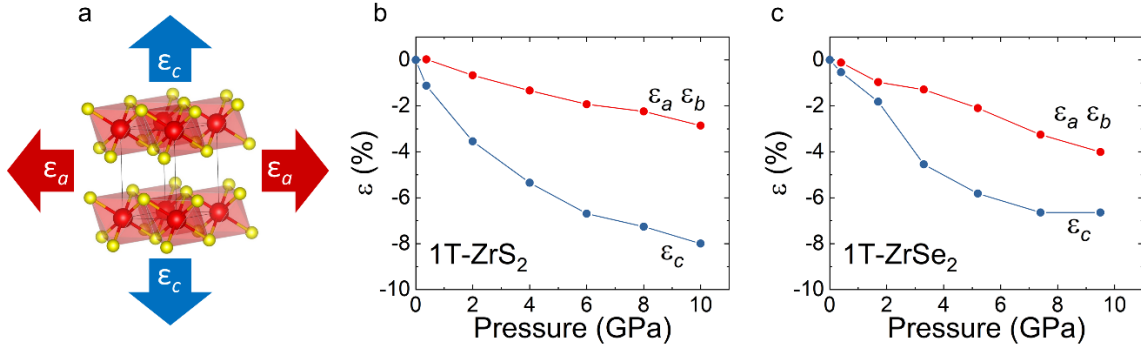
$$\varepsilon_a(P) = \frac{a(P)-a(0)}{a(0)} \cdot 100 \quad (1)$$

Where  $a(0)$  and  $a(P)$  are the same lattice parameter at ambient and pressure  $P$  respectively. Given the hydrostatic conditions of the experiment, only the three diagonal component of the strain tensor are non-zero:  $\varepsilon_a$ ,  $\varepsilon_b$  and  $\varepsilon_c$ . Because of the hexagonal lattice symmetry (P-3m1),

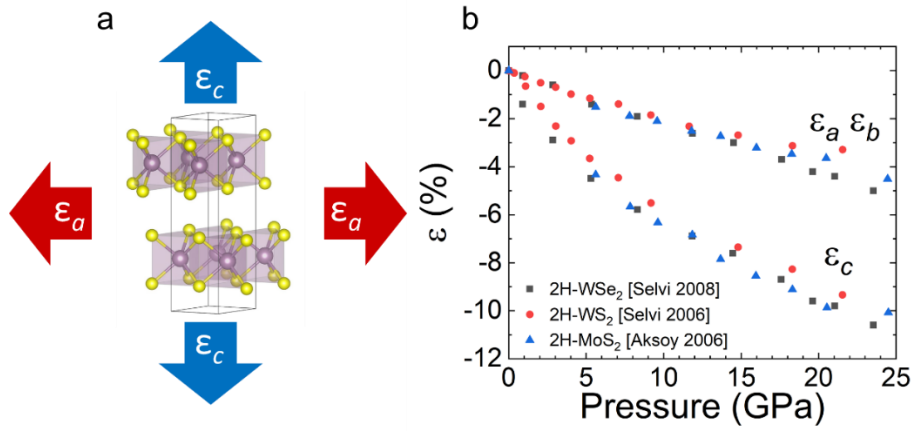
$$\varepsilon_a = \varepsilon_b. \quad (2)$$

As a reference, strain is considered positive when tensile and negative when compressive. In the case of our high-pressure experiments,  $\varepsilon$  is negative as only compressive deformation is produced. In Figure SI 1, we report the computed values, extracted from high-pressure powder XRD for 1T- $\text{ZrS}_2$  and 1T- $\text{ZrSe}_2$ . As a comparison, Figure SI 2 shows the compressibility as function of pressure for the semiconducting 2H polytypes ( $\text{MoS}_2$ ,  $\text{WS}_2$  and  $\text{WSe}_2$ ), computed from published results [11,12,13].

From our results the 1T polytypes appear to have a much higher compressibility than the 2H polytypes. In comparison, at 10 GPa, in-plane strain are  $\varepsilon_a=3.6\%$  and  $\varepsilon_a=2.2\%$  for 1T and 2H respectively. For both materials, the out-of-plane compressibility is much higher than the in-plane one, as one would expect considering the much weaker van der Waals interaction.



**Figure SI 3.** **a)** 1T-ZrX<sub>2</sub> unit cell. The arrows point in the direction of positive strains (tensile) along 2 principal directions,  $\epsilon_a$  is in-plane and  $\epsilon_c$  is out-of-plane. **b)** Experimentally determined pressure-strain relation for 1T-ZrS<sub>2</sub>. **c)** Experimentally determined pressure-strain relation for 1T-ZrSe<sub>2</sub>.

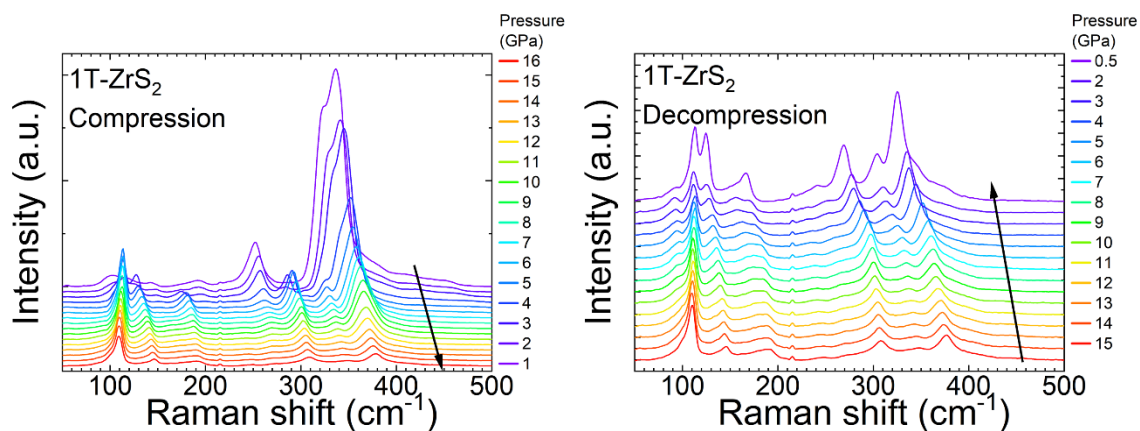


**Figure SI 4.** **a)** 2H-MeX<sub>2</sub> unit cell. The arrows point in the direction of positive strains (tensile) along 2 principal directions. **b)** Experimentally determined pressure-strain relation for 2H-MoS<sub>2</sub>, 2H-WS<sub>2</sub> and 2H-WSe<sub>2</sub>.

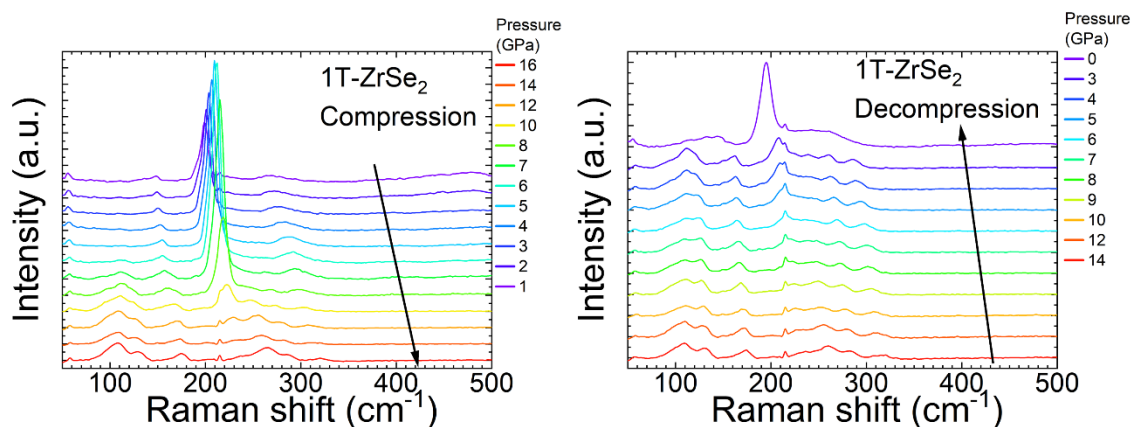


## High-pressure Raman scattering

Here we show the Raman spectra at each pressure during compression and decompression.



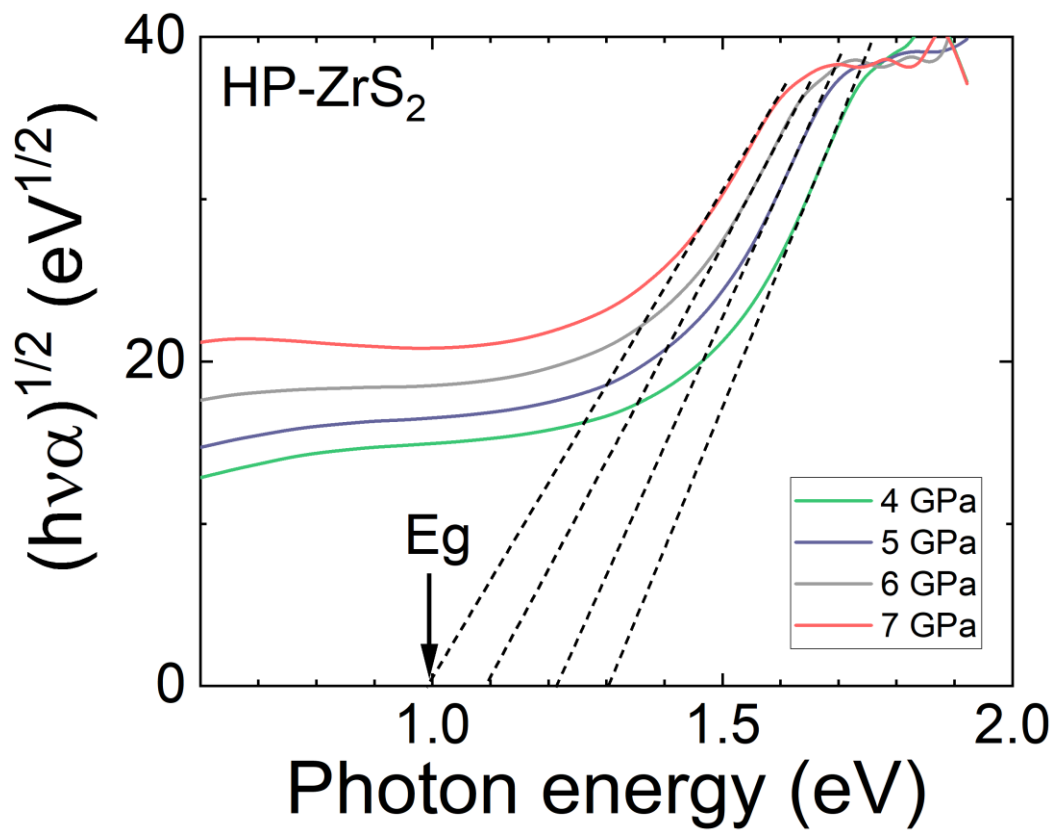
**Figure SI 5.** Raman spectra of ZrS<sub>2</sub> collected during compression and decompression. All curves are shifted vertically by an equal amount.



**Figure SI 6.** Raman spectra of ZrSe<sub>2</sub> collected during compression and decompression. All curves are shifted vertically by an equal amount.

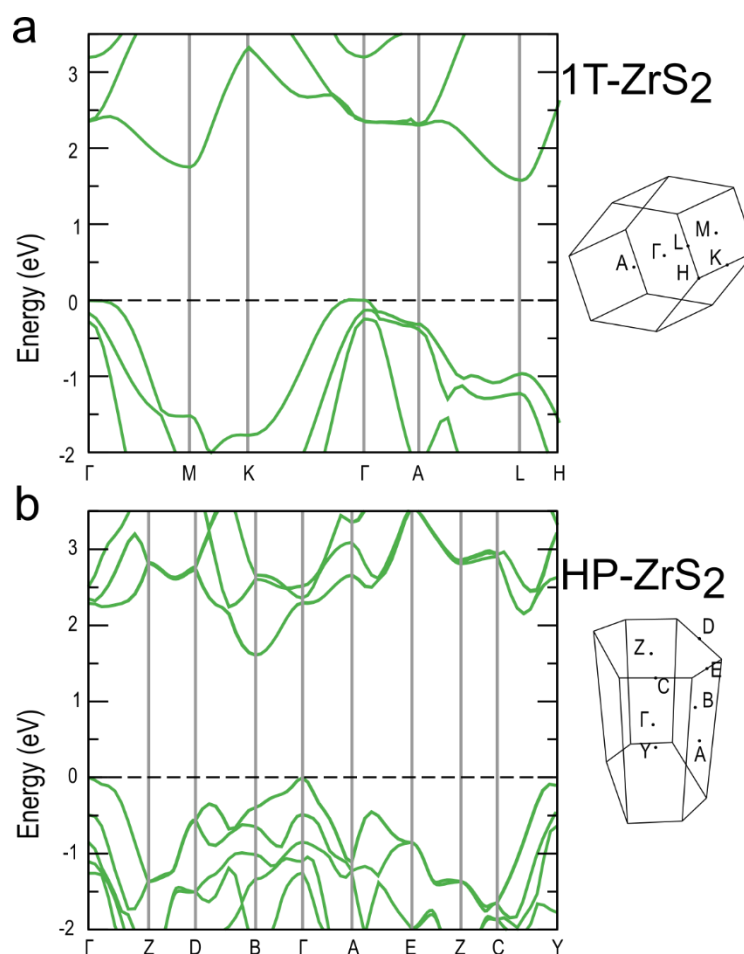
### Band gap estimation from optical transmittance

Values of the optical band gap as a function of pressure were estimated from the optical transmittance data. As all semiconducting phases have an indirect band gap, we used the same empirical model for all data points. After computing the absorption coefficient ( $\alpha$ ) from the experimental data, we estimated the indirect band gap  $E_g$  via linear extrapolations of  $(h\nu\alpha)^{1/2}$ . Representative fitting are shown in Figure SI. 7.



**Figure SI 7.** Representative extrapolation of the indirect band gap for the high-pressure phase of ZrS<sub>2</sub> (HP-ZrS<sub>2</sub>) at different pressures.

## DFT band structures calculations



**Figure SI 8.** Electronic band structure of the (a) low-pressure (0 GPa) and (b) high-pressure (6 GPa) crystalline phases of ZrS<sub>2</sub>, together with the high-symmetry points in the corresponding first Brillouin zones.

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